# **Formation and characterization of oxynitride glasses in the Si-Ca-AI-O-N and Si-Ca-AI,B-O-N systems**

# PAUL E. JANKOWSKI\*,SUBHASH H. RISBUD

*Department of Ceramic Engineering and Materials Research Laboratory, University of Illinois at Urbana-Champaign, Urbana, IL 61801, USA* 

Oxynitride compositions in the Si-Ca-Al-O-N and Si-Ca-Al, B-O-N systems were melted and furnace-cooled in BN crucibles at temperatures from  $\approx$  1650 to 1850 $^{\circ}$ C under dry nitrogen atmospheres. Glass formation, phase stability and crystallization were studied by characterizing the cooled melts by X-ray diffraction, DTA, and electron microscopy. Oxynitride batches with nitrogen content up to  $\approx$  11 at % formed glasses in the Si-Ca-AI-O-N system. Glasses in the Si-Ca-AI, B-O-N system could be formed only when the B<sub>2</sub>O<sub>3</sub> content of the batch was less than  $\approx$  3 wt %. Oxynitride glasses in these boron-containing systems were characteristically inhomogeneous, difficult to process, and prone to crystallization. In both the systems, glasses exhibited glass transitions beginning at  $\approx$  1000° C and crystallization at  $\approx$  1300 to 1500° C. Nitrogen-containing crystalline phases were identified in devitrified glasses via microstructural and micromechanical analyses.

## **1. Introduction**

Burgeoning interest in nitrogen ceramics in the last two decades has resulted in considerable efforts being directed towards the fabrication and properties of  $Si<sub>3</sub>N<sub>4</sub>$  and several multicomponent materials in Si-metal-O-N systems. One of the many fascinating aspects of these developments is the growing enthusiam for investigating a new set of non-crystalline materials generally referred to as oxynitride glasses  $[1-15]$ .

In the present work we have investigated glass formation and stability in the oxynitride systems  $Si-Ca-AI-O-N$  and  $Si-Ca-AI$ ,  $B-O-N$ . The goals were to obtain and characterize glasses in these systems with respect to thermal stability, crystallization, and microstructure.

# **2. Experimental procedures**

### **2.1.** Materials synthesis

Appropriately batched oxide and nitride ceramic 2.2. Materials characterization powders were charged into BN crucibles ( $\approx 2.5$  Materials were characterized by

\*Now at Coming Glass Works, Coming, New York 14830, USA. t!Mode11000A, Astro Industries Inc., Santa Barbara, California, USA.

cm diameter  $\times$  5 cm height) and lightly pressed. The crucible was jacketed by a graphite sleeve and **the** assembly loaded into the chamber of a high temperature graphite element furnace<sup>†</sup> capable of operating up to  $\approx 2500^{\circ}$  C. A schematic sketch of the furnace and the experimental set-up used is shown in Fig. 1. Crucibles were heated in the furnace at  $\approx 30^{\circ}$  C min<sup>-1</sup> under an atmosphere of dry nitrogen (flow rate  $\approx 500 \text{ cm}^3 \text{ min}^{-1}$ ) until the melt processing temperature ( $\approx 1650$ , 1750 or  $1850^{\circ}$  C) was reached. Following a 7h soak at this temperature, the furnace was shut off and allowed to cool. The average cooling rate of the crucible was  $32^{\circ}$ C min<sup>-1</sup> down to  $800^{\circ}$ C, at which time the crucible was removed and quenched in water. Some melts were lowered into a nitrogen glove box and allowed to cool in flowing nitrogen.

differential

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*Figure I* Schematic sketch of the high temperature graphite element furnace used for preparation of oxynitride glasses.

thermal analysis (DTA)\* using  $\approx 10$  mg powdered samples contained in alumina sample cups. DTA traces were obtained in a flowing nitrogen atmosphere at a heating rate of  $10^{\circ}$  C min<sup>-1</sup>.

X-ray diffraction data were obtained on crushed powdered samples at a scan rate of  $1^{\circ}$  min<sup>-1</sup>. Scanning electron microscopy (SEM) and energy dispersive X-ray analysis<sup>†</sup> were conducted on freshly fractured surfaces. SEM images were obtained after etching in a 48% HF acid solution for 15 sec. A thin film of gold was evaporated on the surfaces to reduce charging by the electron beam.

### **3. Results and discussion**

#### 3.1. Melt processing and glass formation

Tables I and II list some of the batch compositions studied for glass formation in the Si-Ca-A1-O-N and Si-Ca-A1, B-O-N systems. It is evident that the batch powders are refractory materials with high melting points.  $SiO<sub>2</sub>$  and  $Al<sub>2</sub>O<sub>3</sub>$  have melting points of  $\approx$  1720 and 2050°C respectively. Cal-

TABLE I Si-CaA1ON compositions

cium nitride,  $Ca<sub>3</sub>N<sub>2</sub>$ , forms a stable liquid at  $1200^{\circ}$  C and is an excellent solvent for aluminium nitride, which does not melt under normal conditions. Processing temperatures of the batches were chosen experimentally in the range  $\approx 1650$ to  $1850^{\circ}$  C. When processed at  $1650^{\circ}$  C, the batch fused, leaving a porous crystalline mass. When exposed to water, particular regions decomposed, suggesting that pockets of unreacted nitride existed in the mass. When soaked at  $1850^{\circ}$ C, the powders melted, and when cooled slowly, resulted in a glass. However, extreme volatilization had occurred during this soak, as evidenced by deposits in the cooler regions of the furnace and the small amount of materials left in the crucible. At  $1750^{\circ}$  C glasses were obtained without excessive volatilization losses, and these compositions are shown in Tables I and II. The BN crucibles are apparently unreactive with the melts since the melt/crucible interface was usually sharp and clean. The glass ingots did adhere to the crucible walls, but usually could be removed by tapping. Si-Ca-A1-O-N glasses were obtained from batches with  $SiO<sub>2</sub>$  contents from  $\approx$  72 to 80 wt %, as shown in Table I. Glasses in this system could not be formed, under the present experimental conditions, when the  $\text{SiO}_2$  in the batch was  $\textless 50 \text{ wt\%}$  or  $\textless 80 \text{ wt\%}$ . The influence of boron on the glass-forming tendency was determined by melting  $B_2O_3$  containing batches (Table II). Glasses formed only when the  $B_2O_3$  content was below approximately 3 wt % but these glasses were often macroscopically inhomogeneous. As the boric anhydride addition increased, the temperature required to melt the batch increased. At approximately 25 wt  $\%$  B<sub>2</sub>O<sub>3</sub> the temperature required to obtain complete melting exceeded  $2050^\circ$  C. At this temperature volatilization losses were extraordinary and devitrification



\*Dupont Model 1090 DTA with 1091 Microprocessor, E. I. Dupont de Nemours, Inc., Wilmington, Delaware, USA. ~JEOL JSM-35C-SEM and Model 595 Scanning Auger Microprobe System (Physical Electronics Industries), Materials Research Laboratory, University of Illinois, Urbana, USA.

Sample number	Composition (wt $\%$ ) as-batched					Nitrogen content	X-ray diffraction
	SiO.	B, O,	AI <sub>2</sub> O <sub>3</sub>	Ca <sub>3</sub> N <sub>2</sub>	AlN	$(at\%)$	identification
8	81.1	3.1	4.5	11.3	-	3.1	<b>Glass</b>
q	74.4	2.8	4.2	10.3	8.3	7.0	Glass
10	73.0	2.8	4.1	10.1	10.1	8.0	Glass
11	50.3	12.6		8.6	28.5	16.0	Crystalline
12	36.0	24.0	23.6	8.2	8.2	6.5	Crystalline

TABLE II Si-CaA1BON compositions

was unavoidable with our experimental procedure. The maximum hatched nitrogen content in the oxynitride glasses studied was  $\approx$  11 at % for a glass in the Si-Ca-Al-O-N system and  $\approx 8$  at % for a glass in the  $Si-Ca-(Al, B)-O-N$  system (Tables I and II). Chemical analyses conducted on selected samples from these systems and other metal-SiA1ON glasses prepared in our laboratory using the same procedure have usually shown that about 60 to 70% of the batched nitrogen is retained in glasses melted at 1700 to  $1750^{\circ}$  C. It is therefore estimated that the maximum values of analysed nitrogen in the samples shown in Tables I and II are  $\approx$  5 at % for the Si-Ca-Al, B-O-N glasses and  $\approx$  7 at % for the Si-CaAlON glasses.

#### 3.2. Thermal analysis (DTA)

Fig. 2 shows representative DTA curves obtained for three glasses. Note that the composition was such that only the nitrogen to oxygen ratio is changed while the calcium, silicon and aluminium concentrations remain the same in these glasses  $(Ca_{3.4}Si_{20.2}Al_{13.5}O_{\nu}N_x)$ . In a number of samples



*Figure 2* Typical DTA traces obtained during heating of Si-Ca-Al-O-N glasses at a heating rate of  $10^{\circ}$  C min<sup>-1</sup>. Note the increase in glass transition and crystallization temperatures with increasing nitrogen content in the glass.

the DTA traces showed multiple peaks (both exotherrnic and endothermic) and the onset of the first endotherm during heating was taken to be the glass transition temperature  $(T_g)$  while the first exotherm was taken to be the crystallization temperature  $(T_c)$ . The  $T_g$  and  $T_e$  values thus obtained are shown in Table III. The trend toward increasing  $T_{\rm g}$  with higher nitrogen content can be seen in Si-Ca-A1-O-N glasses but similar behaviour in the Si-CaAlBON system cannot be easily discerned from the data; this could be due to the inhomogeneity of the boron-containing glasses. The increase in  $T_g$  with nitrogen content has been shown to occur in several Si--M--Al-O--N glasses (where  $M = \text{yttrium}$ , neodymium, calcium and magnesium) by Drew *et al.* [10], in  $Si-Y–Al-O–N$  glasses by Loehman [5] and in a recent study on Si-Ba-A1-O-N glasses by Tredway and Risbud [15]. The  $T_{\rm g}$  values obtained for Si-CaAlON glasses ( $\approx 1000$  to  $1080^{\circ}$ C) in the present study are higher than the  $T_g$  data reported by Drew *et al.* [10] ( $\approx 825$  to 900°C) and could be attributed to differences in the Ca : A1: Si ratios in the two studies. Drew *et al.* [10] studied  $Ca_{18}Si_{18}$  Al<sub>6</sub>O<sub>y</sub>N<sub>x</sub> glasses while our glasses were based on  $Ca_{3.4}Si_{20.2}Al_{13.5}O_yN_x$  compositions.

Fig. 2 also shows increases in the values of  $T_e$ with nitrogen content and while an increase is observed in some cases, the multiple  $T_e$  peaks

TABLE III Glass transition  $(T_g)$  and crystallization  $(T_o)$ temperatures of Si-CaA1ON and Si-CaA1BON glasses

Sample number*	Nitrogen content $(at \%)$	$T_{\rm g}$ (°C)	$T_c$ (°C)
	0	998	1320
	2.0	1000	1380
2	6.5	1032	1420
3	7.9	1080	1445
4	8.5	1080	1408
8	3.1	935	1440
9	7.0	1060	1443
10	8.0	975	1352

\*Refer to Tables I and II.

make it difficult to establish a definite trend. Nevertheless, the  $T_c$  values are usually near  $\approx 1400^{\circ}$  C for oxynitride glasses of both systems studied in this work. These are higher by  $\approx 300^{\circ}$  C in comparison with the  $T_c$  values reported by Drew *etaL* [10].

# 3.3. Microscopy

Si-CaA1ON glasses were generally homogeneous although phase separation was observed after heat treatment. Si-CaA1BON glasses were, however, quite inhomogeneous and often showed macroscopic segregation of metallic particles. Fig. 3 shows a micrograph of a polished cross-section of a glass (Sample 9, Table II) in the Si-Ca-A1BON system. Extensive inhomogeneity was evident in this sample, including regions of dark blue-grey colouration and some faint brown regions in the centre of the melt. Cracks developed during cooling can also be seen in Fig. 3.

The macroscopic droplet formation ( $\approx 0.2$  cm across), marked 3 in Fig. 3, and other adjacent areas of the sample were analysed by SEM to determine microchemistry. Fig. 4 shows elemental maps of silicon, calcium and aluminium obtained in the vicinity of the droplet region marked 3. The droplet is virtually all silicon and significant silicon concentrations can also be observed in adjacent areas of the sample. Integrated intensities of silicon, calcium and aluminium were obtained at regions marked 1, 2 and 3 in Fig. 3 so that estimates of concentrations at various depths in the melt could be obtained. The calcium concentration showed an increase with melt depth and this behaviour was found along the centre and edges of the crucibles as shown in Fig. 5. Similar analyses showed that the silicon and aluminium concentrations decreased with melt depth (Fig. 5).

# 3.4. Phase separation and crystallization

Heat treated glasses were examined by X-ray diffraction and electron microscopy to characterize the microstructure and phase development. Table IV summarizes the X-ray diffraction data on selected heat treated samples all of which were heated at  $1350^{\circ}$  C for 2 h in the graphite furnace and cooled at normal rates. Fig. 6 is an SEM micrograph showing amorphous phase separation developed in a Si-CaAlON glass with  $\approx$  7.9 at % batched nitrogen (Sample 3, Table I). The size of the separation ranges from 2.88 to  $14.4 \,\mu \text{m}$ . The majority of the phase separated droplets are of the order of 5.76  $\mu$ m. The relatively uniform phase distribution suggests that these glasses



*Figure 3* Micrograph of a cross-section of an inhomogeneous oxynitride glass in the Si-Ca-Al, B-O-N system. 2090





*Figure 4* Elemental maps for silicon, calcium and aluminium obtained in the vicinity of the region marked 3 in Fig. 3.

might be suitable for the development of glassceramics.

Fig. 7 shows the microstructure and microchemistry of a crystallized Si-CaAlON sample with  $\approx 8.5$  at % nitrogen (Sample 4, Table I). X-ray identification had shown the presence of  $Si<sub>2</sub>N<sub>2</sub>O$ crystallites in this sample. When analysed by X-ray energy dispersive spectrometry (EDS) in a scanning auger microprobe the crystalline area of the sample (Fig. 7) showed a nitrogen peak not seen in the spectrum of the glassy area. This may be because most of the nitrogen is used up in the precipitation of  $Si<sub>2</sub>N<sub>2</sub>O$  crystals, or perhaps because the nitrogen content of the glass area is small and thus below the EDS detectability limit.

#### 4. Summary

Oxynitride glasses in Si-CaAION and Si-CaA1BON systems were synthesized by conventional glass melting techniques. Si-CaAION glasses were generally homogeneous but macroscopic inhomo-



*Figure 5* Integrated X-ray intensities of calcium, silicon and aluminium obtained from EDS spectra as a function of distance from the melt surface, C is the melt depth along the centre of the glass ingot, and,  $L$  and  $R$  are distances from the surface along the left and right edges of the glass ingot shown in Fig. 3.

TABLE IV Summary of X-ray diffraction data on some heat treated (1350 $^{\circ}$  C, 2 h) Si-Ca-Al-O-N and Si-Ca-A1, B-O-N glasses

Sample number*	Nitrogen content (at $%$ )	X-ray identification of crystalline peaks
1	2	Unidentifiable phase(s)
$\mathbf{c}$	6.5	Mixture of sillimanite and some other unidentifiable phase(s)
3	7.9	Amorphous pattern
4	8.5	Si, ON,
5	11.2	Si, ON,
8	3.1	$\alpha$ -cristobalite
9	7.0	Not sufficiently crvstalline
10	8.0	Amorphous

\*Refer to Tables I and II.

**geneity was observed in Si-CaA1BON glasses. The glass transition temperatures increased with nitrogen content as in other oxynitride glasses, and nitrogen-containing crystalline phases could be precipitated upon heat treatment of selected glasses.** 

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*Figure 6* SEM micrograph of amorphous phase separation in a heat treated Si-CaAION glass sample (Sample 3, Table I).



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